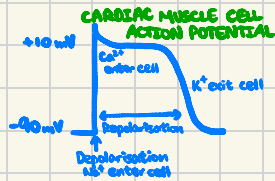


Electrochemical impulses → Contraction of cell

Resting membrane potential (-40 ~ -90 mV)

outside Na^+ Cl^- → Slightly permeable
inside K^+ → Fully permeable



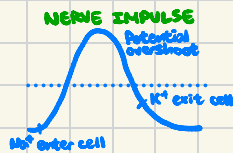
- 1 Depolarisation
- 2 Plateau Phase
- 3 Repolarisation & Contraction

EINTHOVEN TRIANGLE

Lead I: $V_z = \phi_L - \phi_R$

Lead II: $V_z = \phi_F - \phi_R$

Lead III: $V_z = \phi_F - \phi_L$

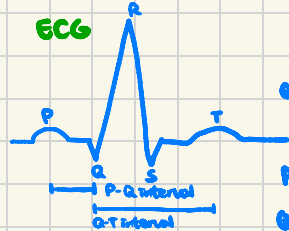


ELECTRO-CONDUCTION PATHWAY

- Sinusatrial node
- Right atrium
- Left atrium
- Atrioventricular node
- Bundle of His
- Right bundle branches
- Left bundle branches
- Purkinje network / fibres

12 LEAD CLINICAL ECG

- Bipolar limb leads
- Augmented unipolar limb leads
- Unipolar (+) chest leads
- Posterior anterior: V_1, V_2, V_3
- Lateral: V_4, V_5, V_6

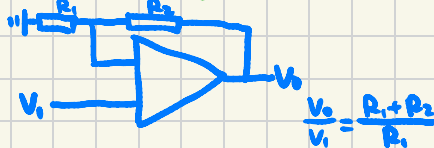


- ECG measures electric currents produced during the cardiac cycle from APs
- Electrodes detect voltage from APs and muscular events

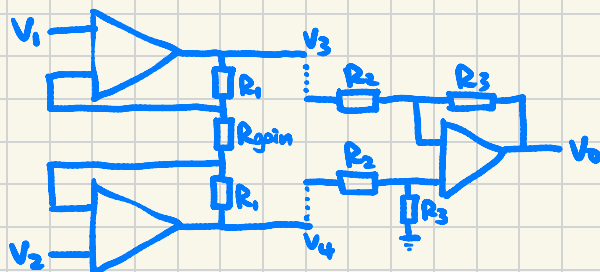
INVERTING AMPLIFIER



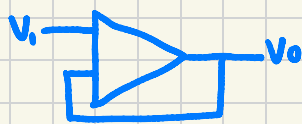
NON-INVERTING AMPLIFIER



INSTRUMENTAL AMPLIFIER



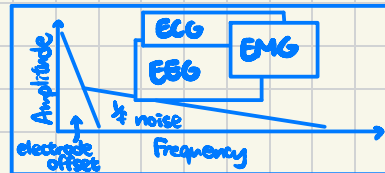
BUFFER/FOLLOWER



- ∴ No current
- ∴ No voltage loss
- ∴ No input Impedance

$V = \frac{E}{d}$
 $C = \frac{Q}{V} = \frac{q}{d}$

- Put in-between skin & ECG to prevent loading error (voltage drop) due to skin impedance
- ~ Get voltage without current / load

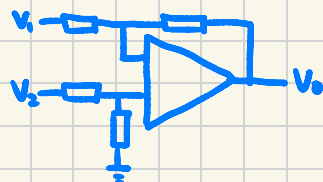


$G_c = 1$
 $V_o = (V_2 - V_1) \left(1 + \frac{2R_1}{R_{gain}}\right) \left(\frac{R_3}{R_2}\right)$

For balanced design: $R_2 = R_3$ → Stage 2 = Differential Amplifier

Let V_3/V_4 for calculations!
Otherwise shit gets weird $\sim (1) \sim$

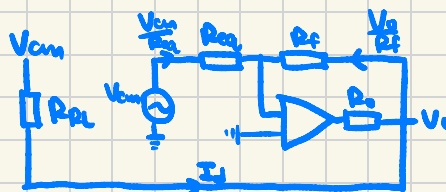
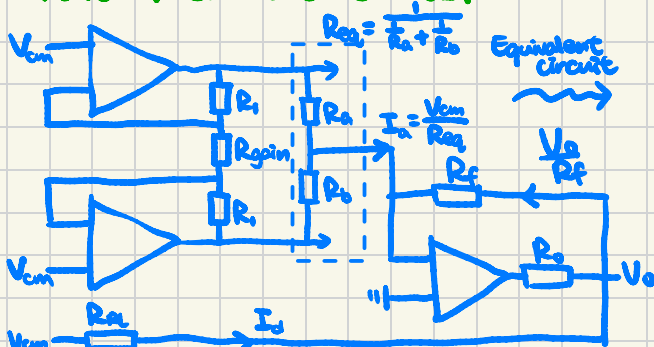
DIFFERENTIAL AMPLIFIER



Common mode
 $V_1 = V_2 = V_i, G_c = \frac{V_o}{V_i}$
Differential mode
 $G_d = \frac{V_o}{V_2 - V_1}$

$CMRR = \frac{G_d}{G_c}$
 $\geq 100/10000$ practically
 $= \infty$ Ideally ($G_c = 0$)

DRIVEN-RIGHT-LEG CIRCUIT

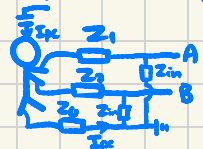


$\frac{V_{cm}}{R_{eq}} + \frac{V_o}{R_f} = 0$
 $V_o = -\frac{R_f}{R_{eq}} V_{cm}$
 $V_{cm} = I_d R_{eq} + V_o$
 $V_{cm} = \frac{R_{eq} I_d}{1 + \frac{R_f}{R_{eq}}}$

INTERFERENCE

- Shield wires
- Coil wires
- ↓ skin-electrode impedance
- ↑ Amplifier input impedance

$V_A - V_B = V_{cm} \left(\frac{Z_{in}}{Z_A + Z_A} - \frac{Z_{in}}{Z_B + Z_B} \right)$
 $V_{cm} = I_{para-cable} Z_{ground}$
 $Z_{in} \gg Z_A / Z_B \Rightarrow V_A - V_B = 0$



Motor unit AP

- Triphasic form
- 3~15 ms
- 20~2000 μV

Surface vs Needle electrode

- S: Cross-talk from adj muscles $\Rightarrow$ Poor selectivity
- N: Small pickup area $\Rightarrow$ Individual MU

Neuropathy:

- Difficulty in initiating nerve impulse
- Takes long time to transmit to muscle $\Rightarrow$ EMG scatter & desynchronisation

Test EMG:

- ① At needle insertion
- ② At rest
- ③ Min contraction
- ④ Max contraction

TRANSDUCER

Case: Prevent electric shock

Damping material: Reduce vibration

Improve axial resolution

Piezoelectric crystal: Piezoelectric effect

Matching layer: Acoustic impedance between crystal & skin
Transmit more ultrasound into tissue

ATTENUATION

① ABSORPTION (friction)

- High viscosity
- Long relaxation time
- High frequency

② REFRACTION

$$\frac{\sin \theta_1}{\sin \theta_2} = \frac{v_1}{v_2}$$

③ SCATTERING

④ DIFFRACTION

⑤ INTERFERENCE

⑥ REFLECTION

$$v_{\text{air}} = 330 \text{ ms}^{-1}$$

$$v_{\text{water}} = 1400 \text{ ms}^{-1}$$

$$v_{\text{soft tissue}} = 1540 \text{ ms}^{-1}$$

$$v_{\text{bone}} = 3400 \text{ ms}^{-1}$$

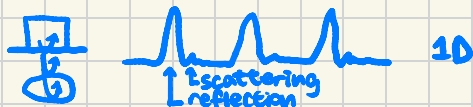
Continuous:

- Doppler flow measurement

Pulse echo:

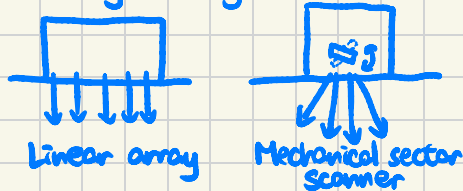
- Imaging

AMPLITUDE MODE (A-MODE)



BRIGHTNESS MODE (B-MODE)

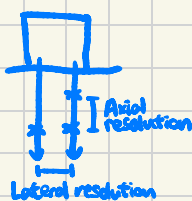
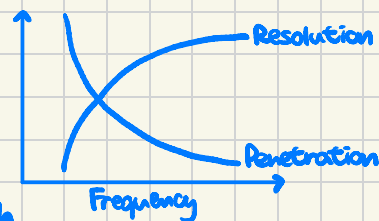
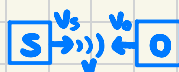
2D image of bright dots



DOPPLER

$$f_D = f_R - f_T$$

$$f' = \frac{v + v_s}{v - v_s} f \cos \theta$$



Axial resolution:

- Spatial pulse length
- Ultrasound frequency

Lateral resolution: (Limiting factor)

- Transducer size
- Beam width

$\therefore v_{\text{bone}} \gg v_{\text{soft tissue}}$

$\therefore$ Image of bone is axially compressed

$\Rightarrow$ Bone distortion

MOTION MODE (M-MODE)

Detailed visualisation of long axis

- Lab-on-a-chip (MEMs/Microfluidics)
- Fluorescence-based DNA Biosensor
- Label-free sensors

- Field effect (charge $\rightarrow$ current) $\rightarrow$ Protein
- Electrochemical (chemical $\rightarrow$ current) $\rightarrow$ Glucose
- Cantilever (mass $\rightarrow$ frequency) $\rightarrow$ Protein

BINDING AFFINITY

$$\frac{d[AB]}{dt} = k_1[A]_s([B]_{\text{max}} - [AB]) - k_2[AB]$$

$$k_1[A][B] = k_2[AB]$$

$$K_d = \frac{k_2}{k_1} = \frac{[A][B]}{[AB]} \text{ (50\% bound)}$$



k_1 : association rate const

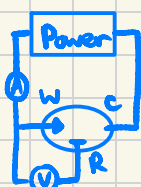
k_2 : dissociation rate const

ELECTROCHEMICAL SENSOR

Enzyme $\rightarrow$ Redox $\rightarrow$ Current

Concentration $\propto$ Rate of reaction $\propto$ Current

- Accurate & Reliable ($\sim$ ppm)
- Power-efficient
- Portable & Easily integrated
- Limited lifespan (2-3 yrs)
- Require calibration against reference
- Sensitive to temperature



Ag/AgCl:

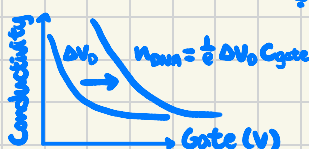
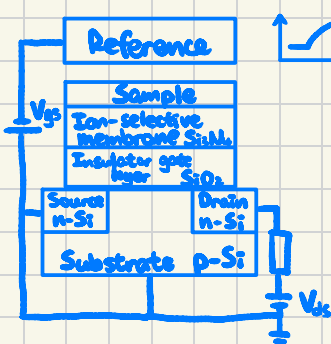
Working electrode

Counter electrode

Reference electrode

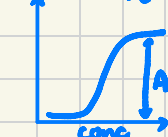
FIELD EFFECT SENSOR

Charge $\rightarrow$ MOSFET $\rightarrow$ Conductivity

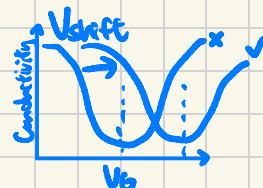
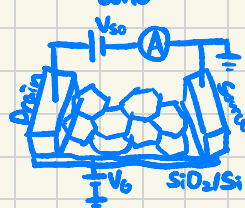


GRAPHENE FIELD EFFECT DNA SENSOR

$$\Delta V_0^{\text{min}} = A \frac{C}{K_d + C}$$



$$\Delta V_0^{\text{min}}(C) = \pm A$$



CANTILEVER SENSOR

